

## Elastic constants.

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Elastic constants characterise the ability of a material to deform under any small stresses. They can be described by a fourth-rank tensor  $C_{ijkl}$ , relating the second-rank stress tensor  $\sigma_{ij}$  to the (also second-rank) strain tensor  $e_{kl}$  via the generalised Hooke's law:

$$\sigma_{ij} = C_{ijkl} \eta_{kl}, \quad \{1\}$$

where multiplication follows the rules of tensor multiplication (see Nye, 1998). Equation  $\{1\}$  can be simplified using the Voigt notation (Nye, 1998), which represents the fourth-rank tensor  $C_{ijkl}$  by a square  $6*6$  matrix  $C_{mn}$ . In these notations, indices '11', '22', '33', '12', '13', '23' are represented by only one symbol – 1, 2, 3, 6, 5, and 4, respectively. These notations significantly simplify all equations. So we write instead of  $\{1\}$ :

$$\sigma_i = C_{ij} \eta_j \quad \{2\}$$

Note that infinitesimal strains are being used; in this limit all definitions of strain (e.g., Eulerian, Lagrangian, Hencky, etc.) become equivalent. Under a small strain, the lattice vectors  $a_{ij}'$  of the strained crystal is obtained from the old lattice vectors  $a_{ij}^0$  and the strain tensor  $e_{ij}$  using the relation:

$$a_{ij}' = (\delta_{ij} + \eta_{ij}) a_{ij}^0. \quad \{3\}$$

In the original tensor notation and in the Voigt notation (Nye, 1998), the  $(\delta_{ij} + e_{ij})$  matrix is represented as follows:

$$\begin{pmatrix} 1+\eta_{11} & \eta_{12} & \eta_{13} \\ \eta_{12} & 1+\eta_{22} & \eta_{23} \\ \eta_{13} & \eta_{23} & 1+\eta_{33} \end{pmatrix} = \begin{pmatrix} 1+\eta_1 & \eta_6/2 & \eta_5/2 \\ \eta_6/2 & 1+\eta_2 & \eta_4/2 \\ \eta_5/2 & \eta_4/2 & 1+\eta_3 \end{pmatrix} \quad \{4\}$$

The Voigt notation allows one to write elastic constants conveniently as a symmetric  $6*6$  matrix. Voigt notation is sufficient in most situations; only in rare situations such as a general transformation of the coordinate system the full fourth-rank tensor representation must be used to derive the transformed elastic constants.

One can define the inverse tensor  $S_{ijkl}$  (or, in Voigt notations,  $S_{ij}^{-1}$ ), often called the elastic compliance tensor:

$$\{S_{ijkl}\} = \{C_{ijkl}\}^{-1} \text{ or } \{S_{ij}\} = \{C_{ij}\}^{-1} \quad \{5\}$$

The  $S_{ij}$  tensor can be defined via the generalised Hooke's law in its equivalent formulation:

$$\eta_i = S_{ij} \sigma_j \quad \{6\}$$

There are two groups of experimental methods of measuring the elastic constants: 1) static and low-frequency methods (based on determination of stress-strain relations for static stresses) and 2) high-frequency, or dynamic, methods (e.g., ultrasonic methods, Brillouin spectroscopy, etc.). High-frequency methods generally enable much higher accuracy. Static measurements yield isothermal elastic constants (timescale of the experiment allows thermal equilibrium to be attained within the sample), high-frequency measurements give adiabatic constants (Belikov *et al.*, 1970). The difference, which is entirely due to anharmonic effects (see below), vanishes at 0 K. Adiabatic  $C_{ij}$  are larger,

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<sup>1</sup> Note that in Voigt notation  $C_{ijkl} = C_{mn}$ , but  $S_{ijkl} = S_{mn}$  only when  $m$  and  $n = 1, 2$ , or  $3$ ; when either  $m$  or  $n = 4, 5$ , or  $6$ :  $2S_{ijkl} = S_{mn}$ ; when both  $m$  and  $n = 4, 5$ , or  $6$ :  $4S_{ijkl} = S_{mn}$  (Nye, 1998).

usually by a few percent. The following thermodynamic equation gives the difference in terms of thermal pressure tensor  $b_{ij}$  (Wallace, 1998):

$$C_{ijkl}^S = C_{ijkl}^T + \frac{TV}{C_V} b_{ij} b_{kl} , \quad \{7\}$$

where  $b_{ij} = (\frac{\partial \sigma_{ij}}{\partial T})_V$  is related to the thermal expansion tensor. For the bulk modulus:

$$K_S = K_T (1 + \alpha \gamma T) = K_T (1 + \frac{\alpha^2 K_T V}{C_V}) \quad \{8\}$$

where  $\alpha$  and  $\gamma$  are the thermal expansion and Grüneisen parameter, respectively.

At constant  $P, T$  the elastic constants describing stress-strain relations {1} are given by:

$$C_{ijkl}^T = \frac{1}{V} (\frac{\partial^2 G}{\partial \eta_{ij} \partial \eta_{kl}})_T \quad \{9\}$$

while at constant P,S they are given by

$$C_{ijkl}^S = \frac{1}{V} (\frac{\partial^2 H}{\partial \eta_{ij} \partial \eta_{kl}})_S \quad \{10\}$$

Now let us derive from {9} an expression for the elastic constants in terms of the second derivatives of the internal energy; in this derivation we follow Ackland and Reed (2003). The unit cell of a crystal can be represented by a matrix  $\overset{\leftrightarrow}{\mathbf{V}} = (\mathbf{a}_1, \mathbf{a}_2, \mathbf{a}_3)$ , and the volume of the equilibrium unit cell is then  $V_0 = \det \overset{\leftrightarrow}{\mathbf{V}}$ . Using {4}, for the volume  $V$  of a strained cell we obtain:

$$\frac{V}{V_0} = \frac{\det \overset{\leftrightarrow}{\mathbf{V}}}{\det \overset{\leftrightarrow}{\mathbf{V}}_0} = 1 + \eta_1 + \eta_2 + \eta_3 + \eta_1 \eta_2 + \eta_2 \eta_3 + \eta_1 \eta_3 - \frac{\eta_4^2}{4} - \frac{\eta_5^2}{4} - \frac{\eta_6^2}{4} + \eta_1 \eta_2 \eta_3 - \frac{\eta_1 \eta_4^2}{4} - \frac{\eta_2 \eta_5^2}{4} - \frac{\eta_3 \eta_6^2}{4} + \frac{\eta_4 \eta_5 \eta_6}{4} \quad \{11\}$$

Then one has in the standard tensor notation:

$$\frac{\Delta V}{V_0} = \eta_{ii} + \frac{1}{4} (2\delta_{ij}\delta_{kl} - \delta_{ik}\delta_{jl} - \delta_{il}\delta_{jk}) \eta_{ij} \eta_{kl} + O(e^3) \quad \{12\}$$

The change of the Gibbs free energy associated with strain is then to the second order:

$$\Delta G = \Delta F + Pe_{ii} + \frac{PV}{4} (2\delta_{ij}\delta_{kl} - \delta_{ik}\delta_{jl} - \delta_{il}\delta_{jk}) \eta_{ij} \eta_{kl} \quad \{13\}$$

From this one has:

$$C_{ijkl}^T = \frac{1}{V} (\frac{\partial^2 F}{\partial \eta_{ij} \partial \eta_{kl}})_T + \frac{P}{2} (2\delta_{ij}\delta_{kl} - \delta_{il}\delta_{jk} - \delta_{jl}\delta_{ik}) \quad \{14a\}$$

and, by analogy,

$$C_{ijkl}^S = \frac{1}{V} (\frac{\partial^2 E}{\partial \eta_{ij} \partial \eta_{kl}})_S + \frac{P}{2} (2\delta_{ij}\delta_{kl} - \delta_{il}\delta_{jk} - \delta_{jl}\delta_{ik}) \quad \{14b\}$$

It is well known (Barron & Klein, 1965; Wallace, 1998) that under non-zero stresses there can be several different definitions of elastic constants. The constants  $B_{ijkl}^T$  and  $B_{ijkl}^S$  defined by equations {14ab} are those appearing in stress-strain relations and in the conditions of mechanical stability of crystals (see below), whereas the long-wavelength

limit of lattice dynamics is controlled by  $\frac{1}{V} \left( \frac{\partial^2 E}{\partial \eta_{ij} \partial \eta_{kl}} \right)_S$ . These two definitions (via stress-strain relations and from long-wavelength lattice dynamics) become identical at zero pressure. Calculating the second derivatives with respect to the finite Lagrangian strains, different equations are obtained (Wallace, 1998).

**ABINIT implementation.** In ABINIT, the so-called “proper” elastic constants are calculated as follows:

$$C_{ijkl}^{proper} = \frac{1}{V_0} \frac{d}{d\eta_{kl}} (V \sigma_{ij}) , \quad \{15\}$$

where  $V_0$  is the volume of the undeformed crystal at given pressure (stress), and  $V$  is the volume changed by strain  $\eta_{kl}$ . Here we have only the first derivative, so only first-order

changes of  $V$  are important (to first order,  $\frac{V}{V_0} = \frac{\det \overset{\leftrightarrow}{\mathbf{V}}}{\det \overset{\leftrightarrow}{\mathbf{V}_0}} = 1 + \eta_1 + \eta_2 + \eta_3$ ). These “proper” elastic

constants do not correspond to the stress-strain definition {1}.

$$\begin{aligned} C_{ijkl}^{proper} &= \frac{1}{V_0} \frac{d}{d\eta_{kl}} (V \sigma_{ij}) = \frac{1}{V_0} \frac{d}{d\eta_{kl}} [V_0 (1 + \eta_{kl} \delta_{kl}) (\sigma_{ij}^0 + C_{ijkl} \eta_{kl})] = \frac{d}{d\eta_{kl}} [\sigma_{ij}^0 + \sigma_{ij}^0 \eta_{kl} \delta_{kl} + O(\eta^2)] = \\ &= C_{ijkl} + \frac{d}{d\eta_{kl}} (\sigma_{ij}^0 \eta_{kl} \delta_{kl}) = C_{ijkl} + \sigma_{ij}^0 \delta_{kl} , \end{aligned} \quad \{16\}$$

where  $\sigma_{ij}^0$  is the stress in the reference structure (for which the elastic constants are being calculated). From {16} the stress-strain defined elastic constants are:

$$C_{ijkl} = C_{ijkl}^{proper} - \sigma_{ij}^0 \delta_{kl} \quad \{17\}$$

In case of hydrostatic pressure ( $P = -\sigma_{11} = -\sigma_{22} = -\sigma_{33}$ ) we obtain corrections only for  $C_{11}$ ,  $C_{22}$ ,  $C_{33}$ ,  $C_{12}$ ,  $C_{13}$ ,  $C_{23}$ , e.g.:  $C_{11} = C_{11}^{proper} + P$ ,  $C_{12} = C_{12}^{proper} + P$ .

At non-hydrostatic conditions, the situation becomes more complicated, in particular the Voigt symmetry ( $C_{ij} = C_{ji}$ ) will be kept only by the “proper” constants – while for stress-strain constants it will be broken, as originally noted by Barron and Klein (1965). For example, from {17}  $C_{41}$  will involve a stress correction, while  $C_{14}$  will not.

[For a systematic treatment of the strain, stress, electrical field and polarisation, see related document “vanderbilt-anaddb-notes.pdf”.](#)

## REFERENCES:

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